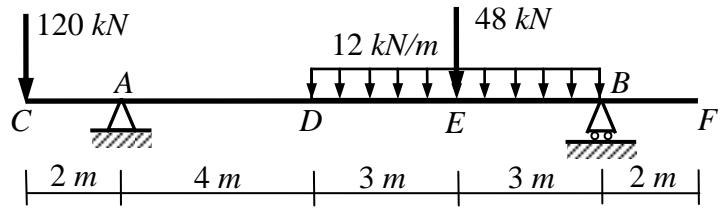


Answer of Final Exam

Question (1): (12 Marks)

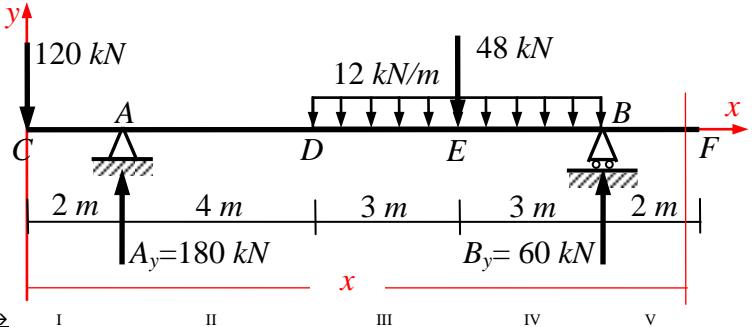
For the shown beam, using the **double integration method**, determine: the deflections at **C**, **D** and **F** and the slope at **C**. Also, sketch the elastic curve of the beam. $EI = 2 \times 10^5 \text{ kN.m}^2$



Solution:

Reactions:

$$\begin{aligned} -120(12) + A_y(10) - (72+48)(3) &= 0 \\ \rightarrow A_y &= 180 \text{ kN} \uparrow \\ 180 + B_y - 120 - 72 - 48 &= 0 \\ \rightarrow B_y &= 60 \text{ kN} \uparrow \end{aligned}$$



$$\begin{aligned} M &= -120x \Big|_I + 180(x-2) \Big|_II - 12(x-6)^2/2 \Big|_III - 48(x-9) \Big|_IV + 60(x-12) + 12(x-12)^2/2 \Big|_V \\ EI y' &= -120x \Big|_I + 180(x-2) \Big|_II - 6(x-6)^2 \Big|_III - 48(x-9) \Big|_IV + 60(x-12) + 6(x-12)^2 \Big|_V \\ EI y' &= -60x^2 \Big|_I + 90(x-2)^2 \Big|_II - 2(x-6)^3 \Big|_III - 24(x-9)^2 \Big|_IV + 30(x-12)^2 + 2(x-12)^3 \Big|_V + C_1 \\ EI y &= -20x^3 \Big|_I + 30(x-2)^3 \Big|_II - 0.5(x-6)^4 \Big|_III - 8(x-9)^3 \Big|_IV + 10(x-12)^3 + 0.5(x-12)^4 \Big|_V + C_1 x + C_2 \end{aligned}$$

Boundary Conditions:

$$\begin{aligned} \text{At } x = 2 \text{ m}, \quad y = 0 \rightarrow 0 &= -20(2)^3 + C_1(2) + C_2 \quad \rightarrow 2C_1 + C_2 = 160 \\ \text{At } x = 12 \text{ m}, \quad y = 0 \rightarrow 0 &= -20(12)^3 + 30(10)^3 - 0.5(6)^4 - 8(3)^3 + 0 + 0 + 12C_1 + C_2 \\ &\rightarrow 12C_1 + C_2 = 5424 \quad C_1 = 526.4 \text{ and } C_2 = -892.8 \end{aligned}$$

So, the general equation of the deflection y at any distance x is,

$$EI y = -20x^3 \Big|_I + 30(x-2)^3 \Big|_II - 0.5(x-6)^4 \Big|_III - 8(x-9)^3 \Big|_IV + 10(x-12)^3 + 0.5(x-12)^4 \Big|_V + 526.4x - 892.8$$

(a) the deflection at C ($x=0$): in Region I:

$$\begin{aligned} EI y_C &= -20(0)^3 - 30(0) + 526.4(0) - 892.8 = -892.8 \\ y_C &= -892.8 / (0.2 \times 10^6) = -0.00446 \text{ m} = -4.46 \text{ mm} \end{aligned}$$

$$y_C = 4.46 \text{ mm} \downarrow$$

the deflection at D ($x=6$): in Region II:

$$\begin{aligned} EI y_D &= -20(6)^3 + 30(4)^3 + 526.4(6) - 892.8 = -134.4 \\ y_D &= -134.4 / (0.2 \times 10^6) = -0.00067 \text{ m} = -0.67 \text{ mm} \end{aligned}$$

$$y_D = 0.67 \text{ mm} \downarrow$$

the deflection at E ($x=9$): in Region III:

$$EI y_E = -20(9)^3 + 30(7)^3 - 0.5(3)^4 + 526.4(9) - 892.8 = -485.7 \rightarrow y_E = -485.7 / (0.2 \times 10^6) = -0.00243 \text{ m} = -2.43 \text{ mm}$$

$$y_E = 2.43 \text{ mm} \downarrow$$

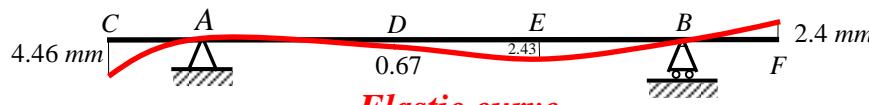
the deflection at F ($x=14$): in Region V:

$$\begin{aligned} EI y_F &= -20(14)^3 + 30(12)^3 - 0.5(8)^4 - 8(5)^3 + 10(2)^3 + 0.5(2)^4 + 526.4(14) - 892.8 \\ &= +476.8 \\ y_F &= 476.8 / (0.2 \times 10^6) = -0.002384 \text{ m} = +2.4 \text{ mm} \end{aligned}$$

$$y_F = 2.4 \text{ mm} \uparrow$$

(b) the slope at C ($x=0$): in Region I:

$$EI y'_C = -60(0)^2 + 526.4 = +526.4 \rightarrow \theta_C = y'_C = +526.4 / (0.2 \times 10^6) \quad \theta_C = +0.002632 \text{ rad} = 0.15^\circ \quad \text{→}$$



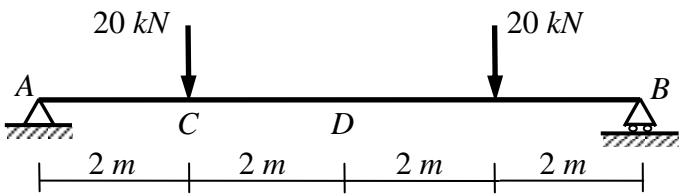
Elastic curve

With my best wishes
Dr. M. Abdel-Kader

Question (2): (12 Marks)

For the shown beam, using the **moment-area method**, determine:

- the slope at **A**
- the deflection at **D**
- the deflection at **C**
and sketch the elastic curve of the beam.
 $E = 400 \text{ GPa}$ and $I = 1300 \text{ cm}^4$



Solution:

$$E = 400 \text{ GPa} = 400 \times 10^6 \text{ kN/m}^2$$

$$I = 1300 \text{ cm}^4 = 1300 \times 10^{-8} \text{ m}^4$$

$$EI = (400 \times 10^6)(1300 \times 10^{-8}) = 5200 \text{ kN.m}^2$$

(a) Slope at A

- Since the slope at **D** (θ_D) is equal to zero, the change in slope between the tangents of the elastic curve at points **A** and **B** (θ_{DA}) is equal to the slope at **A** (θ_A),

$$\theta_{DA} = \theta_D - \theta_A = 0 - \theta_A = -\theta_A$$

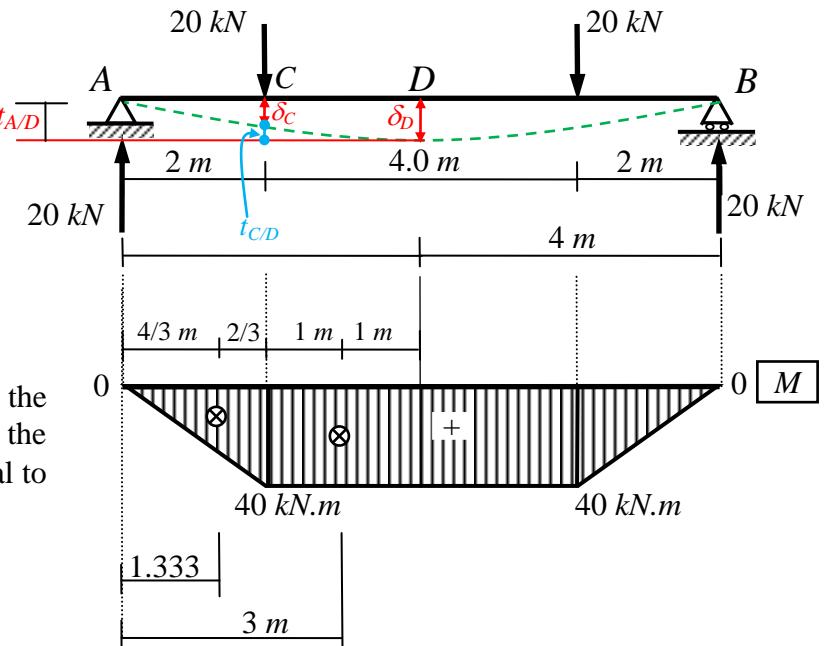
then

$$-\theta_A = \theta_{DA} = \frac{1}{EI} [\text{Area}_{AD}]$$

$$= \frac{1}{5200} [(\frac{1}{2} \times 2 \times 40) + (2 \times 40)] = \frac{120}{5200} = 0.023 \text{ rads}$$

$$\theta_A = -0.023 \times 180/\pi = -1.32 \text{ degrees}$$

$$\therefore \boxed{\theta_A = -1.32^\circ} \quad \text{O}$$



(b) Deflection at D

- The deflection at **D** (δ_D) is equal to the deviation of the point **A** above the tangent to the elastic curve at **D**, then

$$\delta_D = t_{A/D} = \frac{1}{EI} [\text{Area}_{AD} \cdot \bar{x}_A] = \frac{1}{5200} [(\frac{1}{2} \times 2 \times 40)(4/3) + (2 \times 40)(3)] = 0.0564 \text{ m}$$

$$= 0.0564 \times 1000 = 56.4 \text{ mm}$$

$$\therefore \boxed{\delta_D = 56.4 \text{ mm}} \quad \downarrow$$

(b) Deflection at C

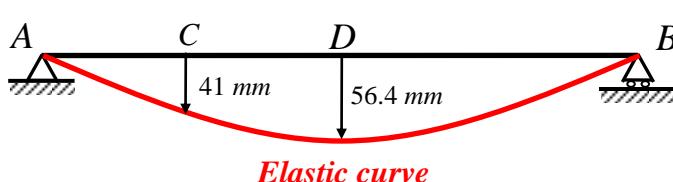
- The deflection at **C** (δ_C) is equal to the deflection at **D** (δ_D) minus the deviation of the point **C** above the tangent to the elastic curve at **D** ($t_{C/D}$), then

$$\delta_C = \delta_D - t_{C/D} = \delta_D - \frac{1}{EI} [\text{Area}_{CD} \cdot \bar{x}_C]$$

$$= 0.0564 - \frac{1}{5200} [(2 \times 40)(1)] = 0.0564 - 0.01538 = 0.04102 \text{ m}$$

$$= 0.04102 \times 1000 = 41.02 \text{ mm}$$

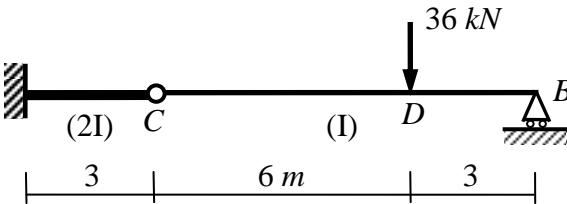
$$\therefore \boxed{\delta_C = 41 \text{ mm}} \quad \downarrow$$



With my best wishes
Dr. M. Abdel-Kader

Question (3): (12 Marks)

For the shown beam of variable cross-section (the relative moments of inertia are given between brackets), using the **conjugate beam method**, determine the slope at **B** and the deflections at **C** and **D**. Also, sketch the elastic curve of the beam. $EI = 20 \times 10^3 \text{ kN.m}^2$



Solution:

Reaction:

$$+\circlearrowleft \sum M_C = 0 : 36(6) - B_y(9) = 0 \rightarrow B_y = 24 \text{ kN} \uparrow$$

$$+\uparrow \sum F_y = 0 : B_y + C_y - 36 = 0 \rightarrow C_y = 12 \text{ kN} \uparrow$$

Construct the bending moment diagram of the real beam. The resulting moment diagram is then loaded to the conjugate beam.

$$W_1 = \frac{1}{2} \times 3 \times 18 = 27 \text{ kN.m}^2$$

$$W_2 = \frac{1}{2} \times 6 \times 72 = 216 \text{ kN.m}^2$$

$$W_3 = \frac{1}{2} \times 3 \times 72 = 108 \text{ kN.m}^2$$

For the conjugate beam, determine the elastic reactions (R_B and R_C) at the supports.

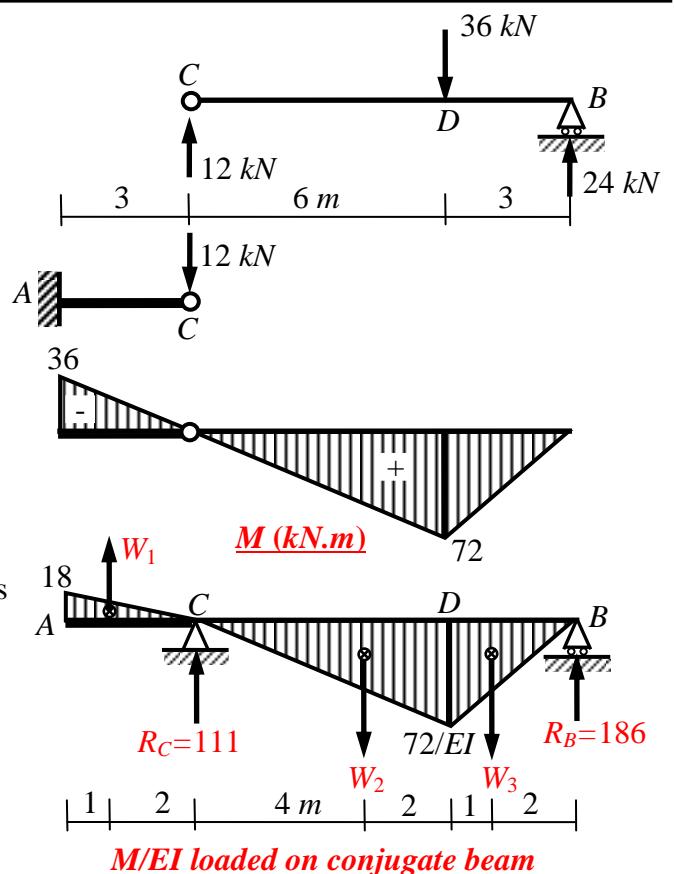
$$+\circlearrowleft \sum M_C = 0$$

$$W_1(2) + W_2(4) + W_3(7) - R_B(9) = 0$$

$$9R_B = 27(2) + 216(4) + 108(7)$$

$$\rightarrow R_B = 186 \text{ kN.m}^2$$

$$+\uparrow \sum F_y = 0 \rightarrow R_C = 111 \text{ kN.m}^2$$



Slope at B

$$\theta_B = -R_B/EI = 186 / 20 \times 10^3 = -0.0093 \text{ rad} = -0.53^\circ$$

$$\boxed{\theta_B = 0.53^\circ}$$

Deflection at C

$$\delta_C = \text{Moment at } C / EI = (W_1 \times 2) / EI = 54 / 20 \times 10^3 = 0.0027 \text{ m} = 2.7 \text{ mm}$$

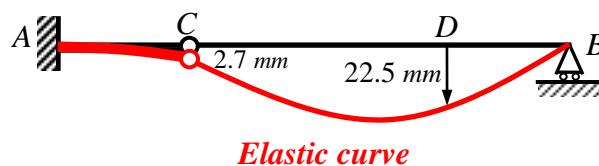
$$\boxed{\delta_C = 2.7 \text{ mm} \downarrow}$$

Deflection at D

$$\delta_D = \text{Moment at } D / EI = (R_B \times 3 - W_3 \times 1) / EI = (186 \times 3 - 108 \times 1) / 20 \times 10^3$$

$$= 0.0225 \text{ m} = 22.5 \text{ mm}$$

$$\boxed{\delta_D = 22.5 \text{ mm} \downarrow}$$



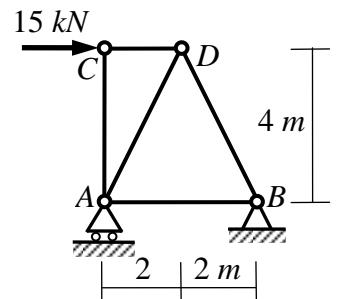
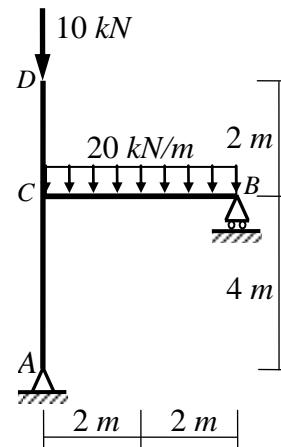
With my best wishes
Dr. M. Abdel-Kader

Question (4): (12 Marks)

For the shown frame and truss, using the **virtual work method**, determine the horizontal displacements at D (δ_{Dh}).

For the frame, $EI = 50 \times 10^3 \text{ kN.m}^2$.

For the truss, assume that all members have the same axial rigidity $EA = 10000 \text{ kN}$.



Solution:

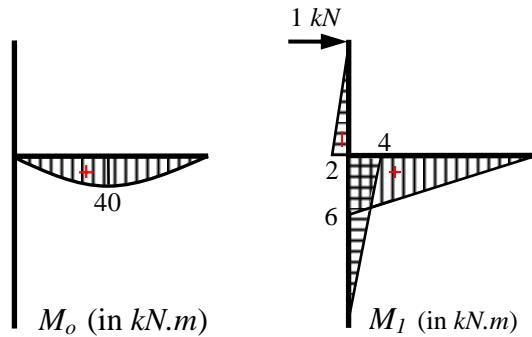
(a) Horizontal displacement at D , δ_{Dh}

- Draw M_o -Diagram due to the applied loads.
- Apply a horizontal load of 1 kN at point D and draw M_1 -Diagram due to this 1 kN load only. then,

$$\delta_{Dh} = \int \frac{M_o M_1}{EI} dL$$

$$\delta_{Dh} = \frac{1}{EI} \left[\left(\frac{2}{3} \times 4 \times 40 \right) \left(\frac{1}{2} \times 6 \right) \right] = \frac{320}{EI}$$

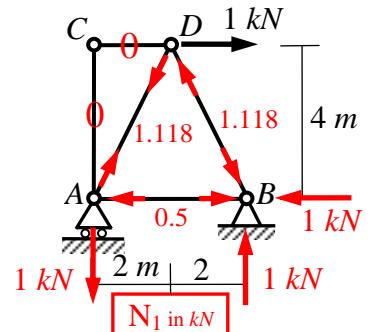
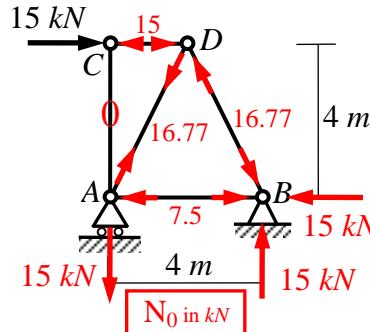
$$\delta_{Dh} = \frac{320}{50 \times 10^3} = 0.0064 \text{ m} = 6.4 \text{ mm}$$



$$\therefore \delta_{Dh} = 6.4 \text{ mm} \rightarrow$$

(b) Horizontal displacement at D , δ_{Dh}

- Calculate N_0 due to the applied loads.



For N_0

$$\text{Joint } D: \rightarrow \sum F_x = F_{DB} (0.4472) - F_{DA} (0.4472) + 15 = 0 \\ \therefore F_{DB} - F_{DA} = -33.54 \quad \dots (1)$$

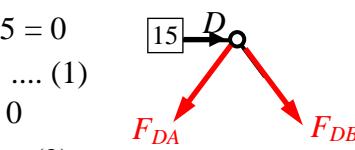
$$+ \uparrow \sum F_y = -F_{DB} (0.8944) - F_{DA} (0.8944) = 0 \\ \therefore F_{DB} = -F_{CA} \quad \dots (2)$$

$$\text{From (1) in (2)} \quad F_{DA} = 16.77 \text{ and } F_{DB} = -16.77$$

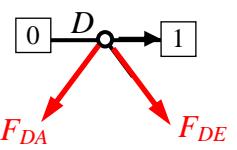
$$\therefore [F_{DA} = 16.77 \text{ T}] \text{ and } [F_{DB} = 16.77 \text{ C}] \quad \dots \text{ and so on}$$

then,

$$\delta_{Dh} = \sum \frac{N_0 N_1 L}{EA} \\ = \frac{(2 \times 16.77 \times 1.118 \times 4.472 + 7.5 \times 0.5 \times 4)}{10000}$$



Joint D for N_0



Joint D for N_1

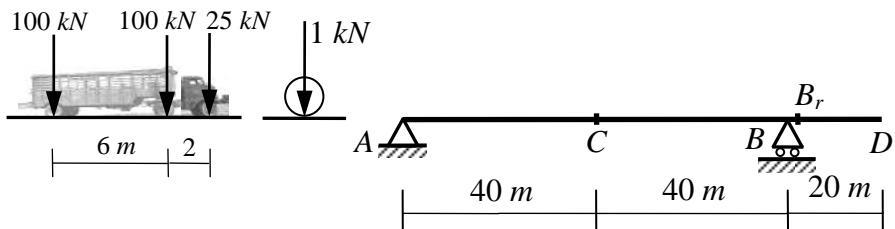
$$= 0.01827 \text{ m} = 18.27 \text{ mm} \quad \therefore \delta_{Dh} = 18.3 \text{ mm} \rightarrow$$

Question (5): (12 Marks)

For the shown beam, draw the influence lines for:

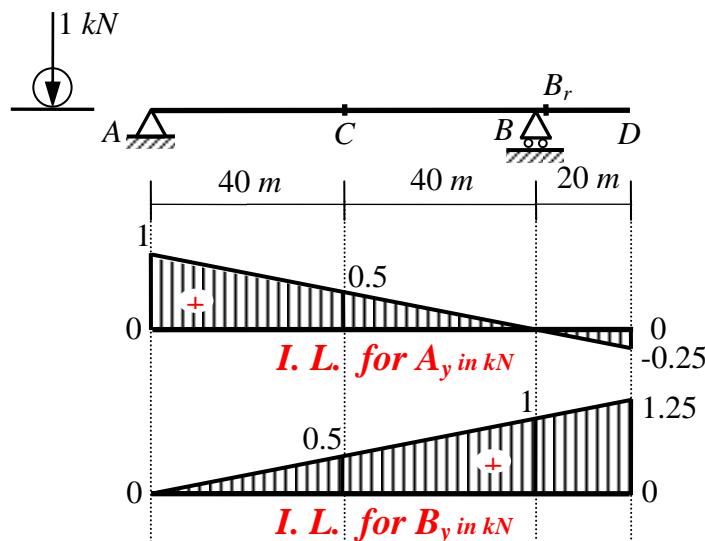
- the reactions A_y , B_y .
- the shear forces at C and B_r .
- the bending moment at C

Also, determine the maximum positive moment at C caused by the shown moving truck.

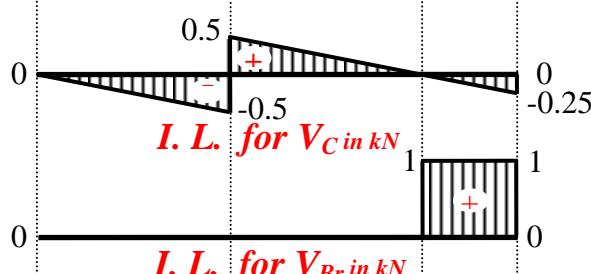


Solution:

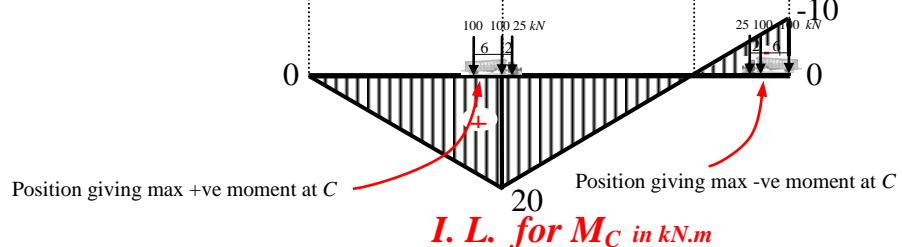
(a)



(b)



(c)



$$M_{D \max +ve} = 100(0.85 \times 20) + 100(20) + 25(0.95 \times 20) = 4175 \text{ kN.m} \quad \text{↑↑}$$

$$M_{D \max +ve} = 4175 \text{ kN.m} \quad \text{↑↑}$$

$$M_{D \max -ve} = 100(-10) + 100(0.7 \times -10) + 25(0.6 \times -10) = 1850 \text{ kN.m} \quad \text{↓↓}$$

$$M_{D \max -ve} = 1850 \text{ kN.m} \quad \text{↓↓}$$

With my best wishes
Dr. M. Abdel-Kader