

Final Exam

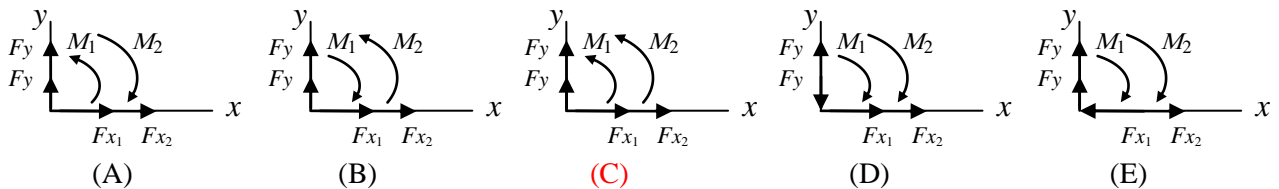
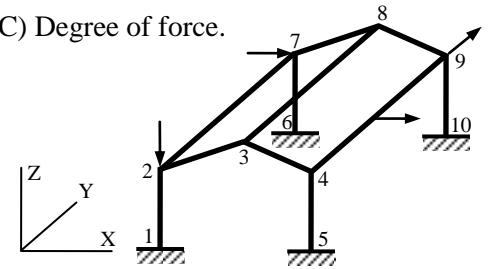
Total Marks: 60

No. of Questions: 3 (Attempt all questions)

Question (1): (20 Marks)

Choose the nearest correct answer (Put A, B, C, D or E in front of the statement number in your answer paper).

- The responsibility of the analytical model results lies on:
(A) The company developed the software. (B) The computer used. (C) The input data.
(D) **The structural designer who used the software.** (E) The structural designer who developed the software.
- The abbreviation "CAD" means:
(A) Common Analysis Data. (B) Computer And Data. (C) Calculation And Design.
(D) **Computer-Aided Design.** (E) Computer-Aided Data.
- The abbreviation "DOF" means:
(A) Possible translations at nodes. (B) Possible rotations at nodes. (C) Degree of force.
(D) **Possible displacements at nodes.** (E) Deformation of forces.
- The number of non-zero DOF for the shown space frame is:
(A) 60 (B) 30 (C) **36** (D) 18 (E) 10
- The number of non-zero DOF per node 1 in the shown space frame is:
(A) **Zero** (B) 1 (C) 2 (D) 3 (E) 6
- The number of non-zero DOF per node 2 in the shown space frame is:
(A) Zero (B) 3 (C) 4 (D) **6** (E) 5
- If the axial deformation is neglected, the number of non-zero DOF per node 2 in the shown space frame is:
(A) 4 (B) 3 (C) **5** (D) 2 (E) 6
- When there are loads between the nodes, the equilibrium equation of a plane frame is $\{F\} = [K]\{\Delta\} + \{F^f\}$ where;
(A) **$\{F\}$ is the nodal forces.** (B) $\{F^f\}$ is the nodal displacements. (C) $[F^f]$ is the element stiffness matrix.
(D) $\{\Delta\}$ is the nodal forces. (E) $[K]$ is square of an order equal to the number of members.
- In 2D Analysis, can be used.
(A) only 2D elements (B) 1D, 2D and 3D elements (C) 2D and 3D elements
(D) **1D and 2D elements** (E) 1D and 3D elements
- Structures that cannot be modeled with the frame element are:
(A) Space frames. (B) Space trusses. (C) **Flat slabs.** (D) Plane frames. (E) Beams.
- Stiffness is the property of an element which is defined as:
(A) Displacement per unit area. (B) Displacement per unit force. (C) **Force per unit displacement.**
(D) **Force per unit displacement.** (E) Force per unit mass.
- For plane frame element 1-2 (connecting joints 1 and 2), the positive sign of forces (forces and moments) is:

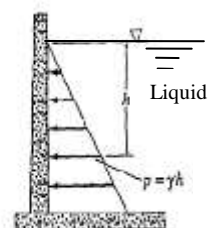


- One of the assumptions that the stiffness method is based on to analyze plane frames is:
(A) Members will behave in non-linear and plastic manner.
(B) Members (beams and columns) are straight with variable properties between joints.
(C) **Axial forces in members are very much less than the respective Euler buckling loads.**
(D) Applied loads may act out of the structure plane.
(E) Deflections are sufficiently large for the changes of geometry to be ignored.

- In SAP, loads and properties of material are:
(A) Fixed data. (B) Output data. (C) **Input data.** (D) Not important.
(E) Results of the analysis

- In SAP, the must be defined for (1D) plane frame elements.
(A) Areas (B) Thicknesses (C) **Sections** (D) Volumes (E) Colors

- The triangle load applied on the shown vertical wall is called load.
(A) Earth pressure (B) Earthquake (C) Settlement (D) Temperature (E) **Hydrostatic**



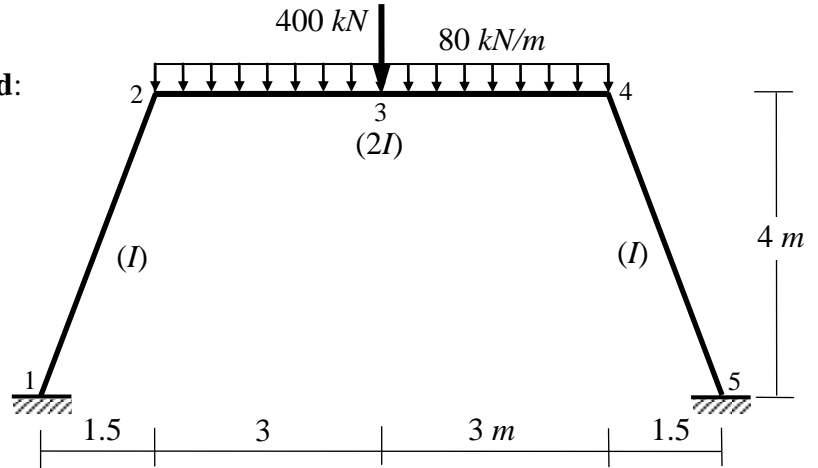
17. In SAP, loads and properties of material are:
 (A) Fixed data. (B) Output data. (C) Results of the analysis. (D) Not important. (E) Input data.
18. In SAP, self-weight loading always acts in the ... direction.
 (A) X (B) Y (C) -Y (D) Z (E) -Z
19. Wind load applied over the height of high rise buildings is assumed:
 (A) Constant. (B) 1000 kN/m. (C) Zero. (D) Parallel to the surface. (E) Perpendicular to the surface.
20. When the material properties are independent of the coordinates, the material is:
 (A) Isotropic. (B) Non-linear. (C) Plastic. (D) Wood. (E) Homogeneous.

Question (2): (20 Marks)

For the shown frame, using the stiffness method:
 Neglect axial deformation

- (a) Determine the displacements at the nodes due to the given loads.
 (b) Draw the bending moment diagram.

Note that E and A are constants, and the relative moments of inertia are given between brackets.



$$[K_e] = \begin{bmatrix} \left(\frac{EA}{L} \lambda^2 + \frac{12EI}{L^3} \mu^2 \right) & \left(\frac{EA}{L} \mu \lambda - \frac{12EI}{L^3} \mu \lambda \right) & -\frac{6EI}{L^2} \mu & \left(-\frac{EA}{L} \lambda^2 - \frac{12EI}{L^3} \mu^2 \right) & \left(-\frac{EA}{L} \mu \lambda + \frac{12EI}{L^3} \mu \lambda \right) & -\frac{6EI}{L^2} \mu \\ \left(\frac{EA}{L} \mu \lambda - \frac{12EI}{L^3} \mu \lambda \right) & \left(\frac{EA}{L} \mu^2 + \frac{12EI}{L^3} \lambda^2 \right) & \frac{6EI}{L^2} \lambda & \left(-\frac{EA}{L} \mu \lambda + \frac{12EI}{L^3} \mu \lambda \right) & \left(-\frac{EA}{L} \mu^2 - \frac{12EI}{L^3} \lambda^2 \right) & \frac{6EI}{L^2} \lambda \\ -\frac{6EI}{L^2} \mu & \frac{6EI}{L^2} \lambda & \frac{4EI}{L} & \frac{6EI}{L^2} \mu & -\frac{6EI}{L^2} \lambda & \frac{2EI}{L} \\ \left(-\frac{EA}{L} \lambda^2 - \frac{12EI}{L^3} \mu^2 \right) & \left(-\frac{EA}{L} \mu \lambda + \frac{12EI}{L^3} \mu \lambda \right) & \frac{6EI}{L^2} \mu & \left(\frac{EA}{L} \lambda^2 + \frac{12EI}{L^3} \mu^2 \right) & \left(\frac{EA}{L} \mu \lambda - \frac{12EI}{L^3} \mu \lambda \right) & \frac{6EI}{L^2} \mu \\ \left(-\frac{EA}{L} \mu \lambda + \frac{12EI}{L^3} \mu \lambda \right) & \left(-\frac{EA}{L} \mu^2 - \frac{12EI}{L^3} \lambda^2 \right) & -\frac{6EI}{L^2} \lambda & \left(\frac{EA}{L} \mu \lambda - \frac{12EI}{L^3} \mu \lambda \right) & \left(\frac{EA}{L} \mu^2 + \frac{12EI}{L^3} \lambda^2 \right) & -\frac{6EI}{L^2} \lambda \\ -\frac{6EI}{L^2} \mu & \frac{6EI}{L^2} \lambda & \frac{2EI}{L} & \frac{6EI}{L^2} \mu & -\frac{6EI}{L^2} \lambda & \frac{4EI}{L} \end{bmatrix}$$

Where, $\lambda = \cos \alpha$ and $\mu = \sin \alpha$

Question (3): (20 Marks)

For the shown truss, using the stiffness method:

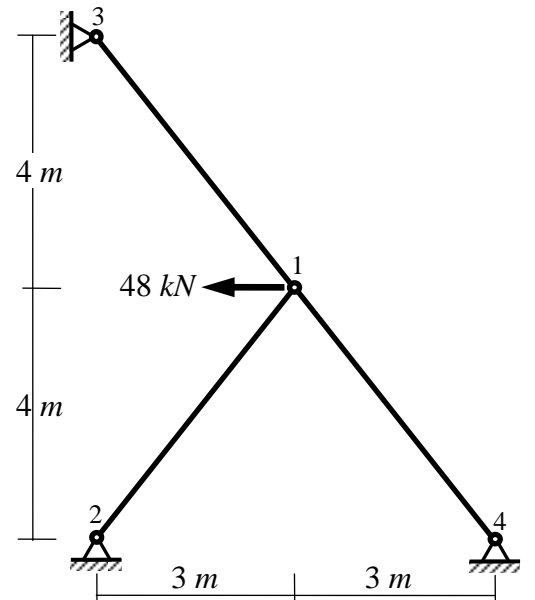
- (a) Determine the displacements at the nodes due to the given loads.
 (b) Determine the reactions at the supports.
 (c) Determine the forces in the members.

Given Data:

EA is constant for all members.

$$[K_e] = \begin{bmatrix} \frac{EA}{L} \lambda^2 & \frac{EA}{L} \mu \lambda & -\frac{EA}{L} \lambda^2 & -\frac{EA}{L} \mu \lambda \\ \frac{EA}{L} \mu \lambda & \frac{EA}{L} \mu^2 & -\frac{EA}{L} \mu \lambda & -\frac{EA}{L} \mu^2 \\ -\frac{EA}{L} \lambda^2 & -\frac{EA}{L} \mu \lambda & \frac{EA}{L} \lambda^2 & \frac{EA}{L} \mu \lambda \\ -\frac{EA}{L} \mu \lambda & -\frac{EA}{L} \mu^2 & \frac{EA}{L} \mu \lambda & \frac{EA}{L} \mu^2 \end{bmatrix}$$

Where, $\lambda = \cos \alpha$ and $\mu = \sin \alpha$



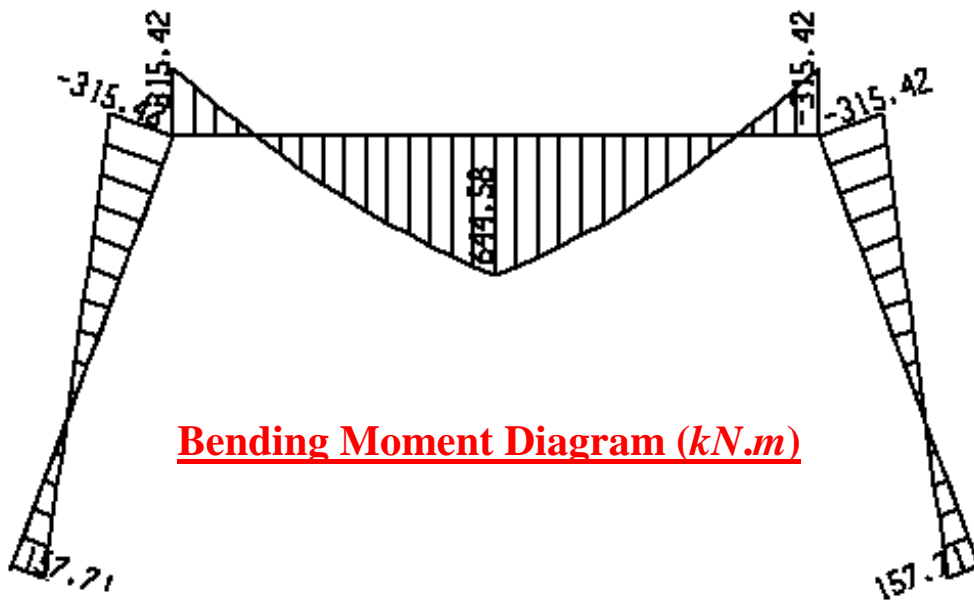
With my best wishes

Dr. M. Abdel-Kader

Question (1): (10 Marks)

Choose the correct answer (Put A, B, C, D or E in front of the statement number in your answer paper).

1.	D		11.	C or D
2.	D		12.	C
3.	D		13.	C
4.	C		14.	C
5.	A		15.	C
6.	D		16.	E
7.	C		17.	E Repeated
8.	A		18.	E
9.	D		19.	E
10.	C		20.	E

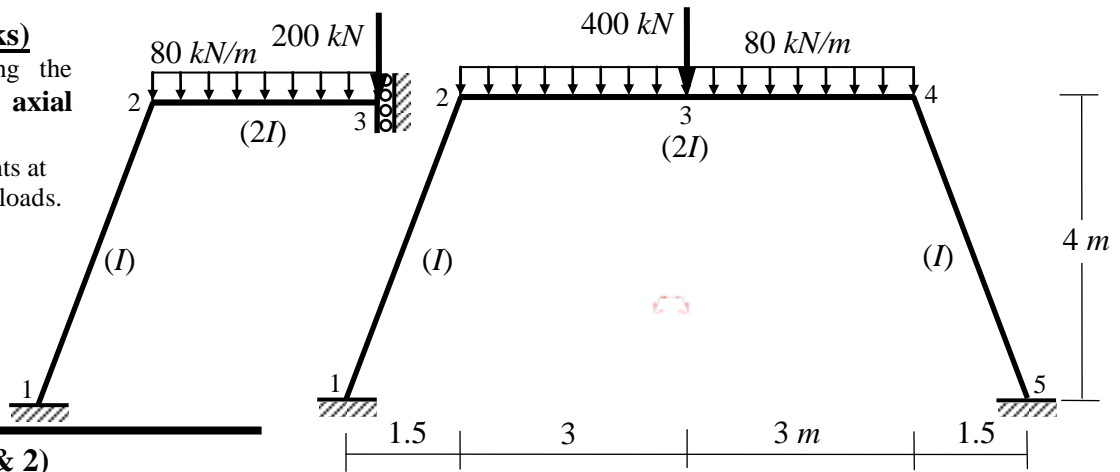


Question (2): (20 Marks)

For the shown frame, using the stiffness method: **Neglect axial deformation**

- (a) Determine the displacements at the nodes due to the given loads.
- (b) Draw the bending moment diagram.

Note that E and A are constants, and the relative moments of inertia are given between brackets.



Element (1): (nodes 1 & 2)

$\lambda = \cos \alpha = 1.5/4.272 = 0.351124$ and $\mu = \sin \alpha = 4/4.272 = 0.93633$

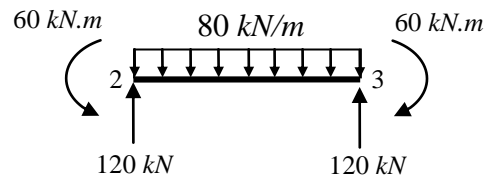
$6EI/L^2 \mu = 6 \times EI / (4.272)^2 \times (0.93633) = 0.307835EI$

$6EI/L^2 \lambda = 6 \times EI / (4.272)^2 \times (0.0351124) = 0.115438EI$

$2EI/L = 2EI/4.272 = 0.468165EI$

$4EI/L = 4EI/4.272 = 0.93633EI$

$$\begin{Bmatrix} X_1 \\ Y_1 \\ M_1 \\ F_{x2} \\ F_{y2} \\ M_2 \end{Bmatrix} = \begin{bmatrix} - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \end{bmatrix} \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ \theta_2 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$



Fixed End Solution

Element (2): (nodes 2 & 3)

$\lambda = \cos \alpha = 1$ and $\mu = \sin \alpha = 0$

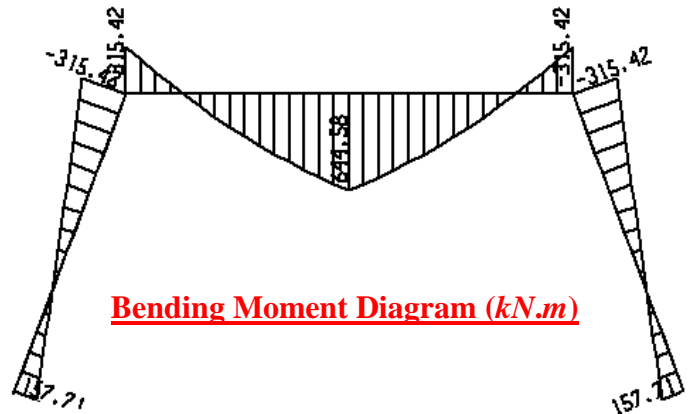
$12EI/L^3 = 12 \times E(2I) / 3^3 = 0.888888EI = 8/9EI$

$6EI/L^2 = 6 \times E(2I) / 3^2 = 1.333333EI = 4/3EI$

$4EI/L = 4 \times E(2I) / 3 = 2.666667EI = 8/3EI$

$2EI/L = 2 \times E(2I) / 3 = 1.333333EI = 4/3EI$

$$\begin{Bmatrix} F_{x2} \\ F_{y2} \\ M_2 \\ F_{x3} \\ F_{y3} \\ M_3 \end{Bmatrix} = \begin{bmatrix} - & - & 0 & - & 0 & - \\ - & - & 4/3EI & - & -8/9EI & - \\ - & - & 8/3EI & - & -4/3EI & - \\ - & - & 0 & - & 0 & - \\ - & - & -4/3EI & - & 8/9EI & - \\ - & - & 4/3EI & - & -4/3EI & - \end{bmatrix} \begin{Bmatrix} 0 \\ 0 \\ \theta_2 \\ 0 \\ v_3 \\ 0 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 120 \\ 60 \\ 0 \\ 120 \\ -60 \end{Bmatrix}$$



Bending Moment Diagram (kN.m)

Frame equation

$$\begin{Bmatrix} X_1 \\ Y_1 \\ M_1 \\ 0 \\ 0 \\ 0 \\ X_3 \\ -200 \\ M_3 \end{Bmatrix} = \begin{bmatrix} - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \\ - & - & - & - & - & - \end{bmatrix} \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ \theta_2 \\ 0 \\ v_3 \\ 0 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 120 \\ 60 \\ 0 \\ 120 \\ -60 \end{Bmatrix}$$

From Row No. 6 $\rightarrow 0 = 3.603EI \theta_2 - 4/3EI v_3 + 60$

From Row No. 8 $\rightarrow -200 = -4/3EI \theta_2 + 8/9EI v_3 + 120 \rightarrow \theta_2 = -336.868/EI \text{ rad}$ and $v_3 = -865.3/EI \text{ m}$

From Element 1

$M_1 = 0.468165EI(-336.868/EI) + 0 = -157.71 \text{ kN.m}$

$M_2 = 0.93633(-336.868/EI) + 0 = -315.42 \text{ kN.m}$

From Element 2

$M_2 = 8/3EI(-336.868/EI) - 4/3EI(-865.3) + 60 = +315.42 \text{ kN.m}$

$M_3 = 4/3EI(-336.868/EI) - 4/3EI(-865.3) - 60 = +644.58 \text{ kN.m}$

With my best wishes

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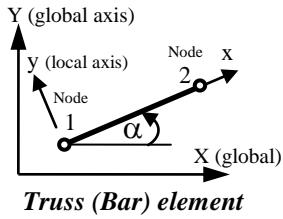
Question (3): (20 Marks)

For the shown truss, using the stiffness method:

- (a) Determine the displacements at the nodes due to the given loads.
- (b) Determine the reactions at the supports.
- (c) Determine the forces in the members.

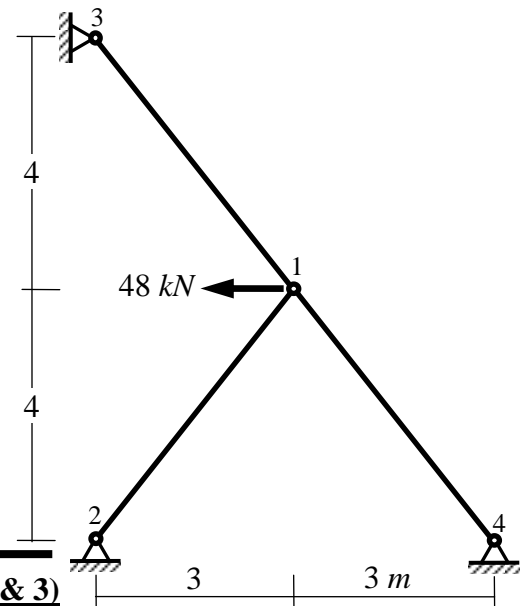
Given Data:

EA is constant for all members.



$$[K_e] = \begin{bmatrix} \frac{EA}{L} \lambda^2 & \frac{EA}{L} \mu \lambda & -\frac{EA}{L} \lambda^2 & -\frac{EA}{L} \mu \lambda \\ \frac{EA}{L} \mu \lambda & \frac{EA}{L} \mu^2 & -\frac{EA}{L} \mu \lambda & -\frac{EA}{L} \mu^2 \\ -\frac{EA}{L} \lambda^2 & -\frac{EA}{L} \mu \lambda & \frac{EA}{L} \lambda^2 & \frac{EA}{L} \mu \lambda \\ -\frac{EA}{L} \mu \lambda & -\frac{EA}{L} \mu^2 & \frac{EA}{L} \mu \lambda & \frac{EA}{L} \mu^2 \end{bmatrix}$$

Where, $\lambda = \cos \alpha$ and $\mu = \sin \alpha$



Element (1): (nodes 1 & 2)

$\lambda = \cos \alpha = -0.6$ and $\mu = \sin \alpha = -0.8$

$EA/L = EA/5 = 0.2 EA$

$$\begin{Bmatrix} F_{x1} \\ F_{y1} \\ F_{x2} \\ F_{y2} \end{Bmatrix} = \begin{bmatrix} 0.072EA & 0.096EA & - & - \\ 0.096EA & 0.128EA & - & - \\ -0.072EA & -0.096EA & - & - \\ -0.096EA & -0.128EA & - & - \end{bmatrix} \begin{Bmatrix} u_1 \\ v_1 \\ 0 \\ 0 \end{Bmatrix}$$

Element (2): (nodes 1 & 3)

$\lambda = -0.6$ and $\mu = 0.8$

$EA/L = EA/5 = 0.2 EA$

$$\begin{Bmatrix} F_{x1} \\ F_{y1} \\ F_{x3} \\ F_{y3} \end{Bmatrix} = \begin{bmatrix} 0.072EA & -0.096EA & - & - \\ -0.096EA & 0.128EA & - & - \\ -0.072EA & 0.096EA & - & - \\ 0.096EA & -0.128EA & - & - \end{bmatrix} \begin{Bmatrix} u_1 \\ v_1 \\ 0 \\ 0 \end{Bmatrix}$$

Element (3): (nodes 1 & 4)

$\lambda = 0.6$ and $\mu = -0.8$ $EA/L = EA/5 = 0.2 EA$

$$\begin{Bmatrix} F_{x1} \\ F_{y1} \\ F_{x4} \\ F_{y4} \end{Bmatrix} = \begin{bmatrix} 0.072EA & -0.096EA & - & - \\ -0.096EA & 0.128EA & - & - \\ -0.072EA & 0.096EA & - & - \\ 0.096EA & -0.128EA & - & - \end{bmatrix} \begin{Bmatrix} u_1 \\ v_1 \\ 0 \\ 0 \end{Bmatrix}$$

Truss equation

	1	2	3	4		
-48	$0.216EA$	$-0.096EA$	$-$	$-$	u_1	
0	$-0.096EA$	$0.384EA$	$-$	$-$	v_1	
X_2	$-0.072EA$	$-0.096EA$	$-$	0	0	0
Y_2	$-0.096EA$	$-0.128EA$	$-$	0	0	0
X_3	$-0.072EA$	$0.096EA$	0	0	0	0
Y_3	$0.096EA$	$-0.128EA$	0	0	0	0
X_4	$-0.072EA$	$0.096EA$	0	0	0	0
Y_4	$0.096EA$	$-0.128EA$	0	0	0	0

From Row No. 1 $\rightarrow -48 = 0.216EA u_1 - 0.096EA v_1$

From Row No. 2 $\rightarrow 0 = -0.096EA u_2 + 0.384EA v_2$

From Row No. 3 $\rightarrow X_2 = -0.072EA (-250/EA) - 0.096EA (-62.5/EA) = 24 \text{ kN}$

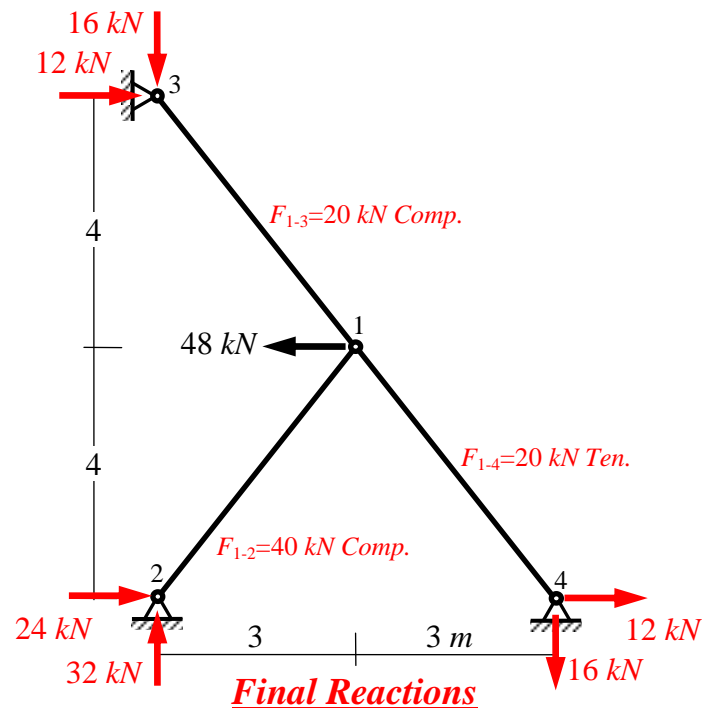
From Row No. 4 $\rightarrow Y_2 = -0.096EA (-250/EA) - 0.128EA (-62.5/EA) = 32 \text{ kN}$

From Row No. 5 $\rightarrow X_3 = -0.072EA (-250/EA) + 0.096EA (-62.5/EA) = 12 \text{ kN}$

From Row No. 6 $\rightarrow Y_3 = 0.096EA (-250/EA) - 0.128EA (-62.5/EA) = -16 \text{ kN}$

From Row No. 7 $\rightarrow X_4 = -0.072EA (-250/EA) + 0.096EA (-62.5/EA) = 12 \text{ kN}$

From Row No. 8 $\rightarrow Y_4 = 0.096EA (-250/EA) - 0.128EA (-62.5/EA) = -16 \text{ kN}$



$u_1 = -250/EA \text{ m}$ ←

$v_1 = -62.5/EA \text{ m}$ ↓

$X_2 = 24 \text{ kN} \rightarrow$

$Y_2 = 32 \text{ kN} \uparrow$

$X_3 = 12 \text{ kN} \rightarrow$

$Y_3 = 16 \text{ kN} \downarrow$

$X_4 = 12 \text{ kN} \rightarrow$

$Y_4 = 16 \text{ kN} \downarrow$